Hydrodynamics and Filtering of Knotted Ring Polymers in Nanochannels

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ABSTRACT: We study the hydrodynamic transport of knotted ring polymers through modulated channels, establishing that the transport velocity is strongly dependent on the ring topology for Peclet numbers smaller than unity. As soon as convection dominates, transport properties become insensitive to the presence and type of knots. We identify two distinct modes of transport, corresponding to the motion being led by the knotted or unknotted portions of the ring, most surprisingly without impact on separation efficiency. The modes can be selected by the channel geometry, and this could be harnessed to design nanofluidic devices for the continuous topological sorting of entangled biopolymers.

1. INTRODUCTION

Channel confinement is increasingly used as the method of choice for examining the impact of topology on the physical behavior of polymers. In recent breakthrough experiments, linear DNA filaments were trapped inside a channel and their metric properties were monitored, while their knotted state was changed by compression or elongation.1–3 The measurements, together with models and simulations, helped establish how the knotting and unknotting kinetics is coupled to the global dynamics of the chain,1–3 how knot size fluctuates in and out of equilibrium,6–8 and how the motion of knots along the confined chains responds to an externally imposed flow or elongational field.2,3 Besides the relevance to polymer physics, these aspects have bearings in applicative contexts such as genomic barcoding, where erroneous readouts can be caused by the backfolded contour of knotted DNA.9 Channel confinement has been applied to ring polymers as well. These systems have been mostly studied for their static properties, and particularly for the nonmonotonic dependence of knotting probability on channel width,6,8 which has been associated with the free energy balance between the knotted and unknotted portions.5,10

By contrast, the rich kinetic behavior of confined knotted rings is still underexplored, and basic properties, such as transport, have remained unclarified. In this work, we examine the unique mobility properties resulting from the combined action of hydrodynamic flow and channel geometry. We use hydrodynamic simulations to study how differently knotted rings flow through channels with a periodic hourglass topography, where chambers, which entropically trap the polymers, and narrowings, which hinder knot passage, appear in alternation. This, as we show, realizes a minimalist system where the diffusive and convective transport components of different knot types can be competitively adjusted via the flow strength or channel geometry. It also allows us to test the hypothesis, based on simulations without hydrodynamics,11 that channel shape can be optimized to make possible the separation of rings with the same length but different knot types, as needed, for example, for topological profiling of viral DNA. Until now, filtering mechanisms for chains and rings have been proposed,12,13 which however are not aimed at discriminating rings by knot type. We demonstrate that the mobility of the rings depends strongly on topology for Peclet numbers smaller than unity. We further establish that transport can occur in two modes: one which is led by the knotted portion of the polymer and the other described by the knotted section trailing behind. These two modes do not affect separation efficiency and are owed to the interplay of constriction radius, knot size, and hydrodynamic backflow. The results provide quantitative criteria and insights that we expect will be useful for designing nanofluidic devices for topological sorting of entangled polymers.

The rest of the article is organized as follows. We introduce the polymer model, the hydrodynamic simulation technique, and the system setup in Section 2. Subsequently, we present equilibrium properties of polymers in Section 3 and their convective transport in such corrugated channels in Section 4. In Section 5, a detailed analysis of knot conformations and modes of translocations is presented, and in Section 6, we summarize and draw our conclusion.

2. MODEL AND SIMULATION DETAILS

We employed a bead-spring model, suitable for flexible ring polymers in a good solvent, consisting of $M = 150$ monomers. Excluded volume interactions between monomers $i$ and $j$ were modeled via the shifted and truncated Weeks–Chandler–Andersen (WCA) potential $U_{\text{WCA}}$.14
\[
U_{\text{WCA}} = \frac{1}{2} \sum_{i=1}^{M} \sum_{j \neq i}^{M} 4 \varepsilon_{\text{MM}} \left( \frac{\sigma_{\text{MM}}}{r_{ij}} \right)^{12} - \left( \frac{\sigma_{\text{MM}}}{r_{ij}} \right)^{6} + \frac{1}{4} \right) \times \Theta(2^{1/6} \sigma_{\text{MM}} - r_{ij})
\]

Here, \( \varepsilon_{\text{MM}} / k_B T = 1 \) is the bead–bead interaction strength, \( k_B T \) is the thermal energy, \( \sigma_{\text{MM}} \) denotes the bead diameter, \( r_{ij} \) is the distance between beads \( i \) and \( j \), and \( \Theta(\cdots) \) is the Heaviside function.

Polymeric bonds between subsequent monomers were accounted for by the finite extensible nonlinear elastic (FENE) potential \( U_{\text{FENE}} \)

\[
U_{\text{FENE}} = \sum_{i=1}^{M} \left( \frac{\sigma_{\text{MM}}}{2} \kappa R_0^2 \ln \left( 1 - \left( \frac{r_{i,i+1}}{R_0} \right)^2 \right) \right) \text{if } r_{i,i+1} \leq R_0
\]

with the standard Kremer–Grest parameters for the bond constant \( k = 30 \varepsilon_{\text{MM}} / \sigma_{\text{MM}}^2 \) and the maximum bond extension \( R_0 = 1.5 \sigma_{\text{MM}} \). Note that in eq 2, if \( i = M \), then \( i + 1 = 1 \), to ensure a closed loop. The interplay of the FENE connectivity term and the excluded volume interaction ensures that the initial topology of the rings is maintained at all times. For the latter, we consider the three simplest types of knots, namely, the unknot (0), the trefoil knot (3), and the figure-of-eight (4) knot (see Figure 1a).

To identify the knotted region, we used the method of refs 18,19, as implemented in the KymoKnot software package. The algorithm identifies the smallest portion of the ring that, after a suitable closure, has the same topology of the entire ring. Tracking this portion during the simulation provides the instantaneous values of knot features, such as the knot contour length, \( l_g \), and the position of its CoM, KCoM. By restricting the sum in eq 3 to the monomers of the knotted subpart of the ring, we calculated the radius of gyration of the knotted region \( R_{gK} \) via eq 4.

The importance of convective versus diffusive polymer transport is captured by the dimensionless Peclet number

\[
P_e = \frac{v_p R_g}{D_p}
\]

In eq 6, \( v_p \) is the average transport velocity of each polymer topology and \( R_g \) and \( D_p \) are the average gyration radius and diffusion coefficient in bulk, respectively. Thus, \( P_e \) changes with the polymer topology at constant flow strength, and for \( P_e < 1 \), a polymer diffuses faster over its characteristic length scale \( R_g \) than being transported convectively over the same distance.

The general setup considered in this study is illustrated in Figure 1b. The system consists of a cylindrical channel with a periodic hourglass modulation, obtained from the mirror juxtaposition of truncated cones. Its geometry is specified by the large and small diameters, \( 2R_{\text{max}} \) and \( 2R_{\text{min}} \), respectively, and by the longitudinal extension of the repeated modular chamber, \( 2l \). The values of \( R_{\text{max}} \) and \( l \) are both set equal to \( 9 a_0 \), with \( a_0 = \sigma_{\text{MM}} \) so as to be larger but comparable to the average gyration radius of unknotted rings in bulk, \( R_g \approx 6.99 \pm 0.08 a_0 \), for the considered chain length. The ratio of polymer volume to chamber volume has been evaluated as optimal scaling conditions \(^{1,21} \) and is the same as for a chain of \( M = 300 \) in the setup of ref 11. Previously, such entropic traps combined with electric fields were used to separate dsDNA by its size but not topology.\(^{22} \) The WCA potential defined in eq 1 is employed for the excluded volume interaction between monomers and the channel wall; in this case, \( r_{ij} \) denotes the distance between monomer \( i \) and the closest point at the channel wall, \( j \). When beads are close to the narrowing, a normal vector to the wall cannot be defined; thus, the length of the shortest vector, which connects the monomer and the constriction, is chosen as the distance.

To include solvent-mediated monomer–monomer and monomer–wall hydrodynamic interactions (HIs), we employed the multiparticle collision (MPC) fluid model.\(^ {23,24} \) This particle-based approach offers the advantage of conserving locally mass, energy, and momentum, thus fulfilling the Navier–Stokes equations while also accounting for thermal fluctuations. As there is no potential acting among MPC fluid particles, fluid particles and walls, as well as fluid particles and monomers, the MPC approach is computationally much less onerous than molecular dynamics (MD) simulations with explicit solvent and allows to bridge the time scales associated with the solvent and solute.\(^ {25} \) Furthermore, many fluid properties, such as transport coefficients, can be calculated analytically.\(^ {26,27} \)

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**Figure 1.** (a) Typical conformations of circular polymers of \( N = 150 \) beads of diameter \( a_0 = \sigma_{\text{MM}} \) and tied with 0, 3, and 4 topologies. (b) The chamber consists of two mirror-symmetric, truncated cones joined on their broad side. The length of a chamber is \( 2l \), the radius of the largest circular section is \( R_{\text{max}} \) and that of the constriction is \( R_{\text{min}} \).

The metric properties of the rings were mostly characterized by employing suitable combinations of the elements of the gyration tensor \( G \)

\[
\hat{G}_{\alpha\beta} = \frac{1}{M} \sum_{i=1}^{M} s_i \alpha \delta_i \beta
\]

Here, \( \alpha \beta \) are the Cartesian components of the bead position, \( s_i \), relative to the polymer’s center of mass (CoM). The gyration radius \( R_g \) is expressed as

\[
R_g = \sqrt{\text{tr}(\hat{G})}
\]

Here, the hat superscript indicates instantaneous values, while no such superscript is used for time-averaged values. In addition to the gyration radius, we also computed the longitudinal span, \( S \). The span provides a measure of the footprint of the ring projected along the channel axis, which is parallel to the \( x \) Cartesian axis, with \( r_i \) being the position of bead \( i \)

\[
S = \max(r_{i,x}) - \min(r_{i,x})
\]
The algorithm evolves in two steps; first, particles are propagated ballistically during the streaming step over a time interval $h$

$$x_i(t + h) = x_i(t) + h\mathbf{v}_i(t)$$  \hspace{1cm} (7)

with $x_i(t)$ and $\mathbf{v}_i(t)$ representing particle’s $i$ position and velocity at time $t$, respectively. Second, momentum between solvent particles is transferred in the collision step. Here, particles are assigned to the cells of length $a_0$, and then the particles’ velocities relative to the CoM velocity $\mathbf{v}_{\text{cell,COM}}$ of a cell are rotated by a fixed angle $\alpha$ around a randomly oriented axis via the rotation operator $\Omega$:

$$\mathbf{v}(t + h) = \mathbf{v}_{\text{cell,COM}}(t) + \Omega_{\text{fl}}[\mathbf{v}(t) - \mathbf{v}_{\text{cell,COM}}(t)]$$  \hspace{1cm} (8)

Conveniently, the particles’ mass $m_p$, the thermal energy $k_B T$, and the length of a cell $a_0$ are set equal to unity, thus defining the natural unit of time, $t_0 = a_0^2/\sqrt{\kappa B}$. The kinematic viscosity of the MPC fluid, a measure of how fast momentum diffuses, is determined by the rotation angle $\alpha = 130^\circ$, the collision time step $h = 0.1t_0$, and the average solvent number density $\rho = 5a_0^{-3}$, yielding a kinematic viscosity $\nu = 0.79a_0^2/t_0$ (dynamic viscosity of $\eta = m_p\nu = 3.96m_p(a_0t_0)$ for the chosen parameter set).

A random grid shift is performed before every collision step to restore Galilean invariance. Liquids are characterized by the dominance of collisional momentum transport compared to diffusive momentum transport, which is expressed by Schmidt numbers larger than unity.25 In our simulations, the Schmidt number $Sc = \nu/\sigma$ was set equal to the size of a collision cell, $\sigma_{\text{MM}} = a_0$ as already noted.

To simulate buoyant beads, the mass of a polymer bead $m_{M}$ is set equal to the average mass of a cell filled with solvent only ($m_{M} = m_p a_0^3 = 5m_p$). During the streaming step of MPC particles, monomers are propagated via MD with a time step $\delta = h/150$; this small time step ensures the conservation of topology. The coupling between the MD and MPC algorithm is accomplished by inclusion of monomers in the collision step.33 To create a flow, a body force $f = m g$ with acceleration $g$ is applied to all solvent particles, leading quickly to a steady-state flow profile. The average fluid flow velocity is directly proportional to the applied body force (see Figure 2). In a geometry with longitudinally varying cross section, flow velocities must be slow so as to ensure that fluid particles can diffusively explore the cross section, which is ensured by the fluid Peclet number $Pe_0 \ll 1$. In our simulations, the maximum $Pe_0 = 0.03$, taking a cell size $a_0$ as the characteristic length. Additionally, we verified that the fluid particle density resolved in radial and longitudinal directions is constant. Furthermore, our simulations result in Mach numbers $Ma \ll 1$, which is the ratio of flow velocity to sound velocity, and $Ma \ll 1$ is a characteristic of a fluid.25 We employed bounce-back rules for solvent particles colliding with the walls to account for stick boundary conditions between fluid and wall, in addition to virtual particles.35 At the midpoints $R(x) = R_{\text{max}}$, multiple reflections of fluid particles at the channel walls can occur, which are accounted for by placing fluid particles to the closest point at the wall and assigning them random velocities in normal and tangential directions to the channel wall, as used in the case of colloids.36 We have adjusted the thickness of the virtual particle layer, such that the combined virtual particle/solvent particle distribution during the random grid shift reproduces a Poisson distribution with an average number of particles $\rho a_0^3$ and the distribution of relative velocities of fluid and solvent particles, following a Maxwell–Boltzmann distribution. The latter is only fulfilled when employing the Maxwellian thermostat,37 as we do.

Error bars are calculated from four simulations started from independent initial configurations. Error propagation is explicitly taken into account. Note that the $3_1$ knot is chiral, thus we initialized an equal number of independent simulations with every enantiomer, although we do not expect any influence of chirality in this setup.

3. EQUILIBRIUM PROPERTIES IN THE BULK AND IN CONFINEMENT

Bulk properties of ring polymers of $M = 150$ monomers bearing $0_1$, $3_1$, or $4_1$ knots are summarized in Table 1, obtained by simulations in a cubic box of size $L = 50a_0$ with periodic boundary conditions. Table 1 indicates the radius of gyration $R_g$ diffusion coefficient $D_{\text{bulk}}$, largest relaxation time $\tau$, which was calculated as the time it takes for a polymer to diffuse over its radius, and the polymer transport velocity at $Pe = 1, \nu_{\text{Pe=l}}$. $R_g$ is a static quantity, in good agreement with Langevin simulation of polymers without solvent,11 whereas diffusivities, a dynamic quantity, are different. This is due to the fact that in Rouse-like dynamics the friction experienced by the polymer is $\zeta = M\zeta_M$ with $\zeta_M$ being the friction coefficient per monomer, thus distinct topologies have the same bulk diffusion

<table>
<thead>
<tr>
<th>knot</th>
<th>$R_g/a_0$</th>
<th>$D_{\text{bulk}}[a_0^2t_0^{-1}]$</th>
<th>$\tau[t_0]$</th>
<th>$\nu_{\text{Pe=l}}[a_0t_0^{-1}]$</th>
</tr>
</thead>
<tbody>
<tr>
<td>$0_1$</td>
<td>6.99 ± 0.08</td>
<td>(1.6 ± 0.2) × 10^{-3}</td>
<td>5090</td>
<td>2.1 × 10^{-3}</td>
</tr>
<tr>
<td>$3_1$</td>
<td>6.11 ± 0.05</td>
<td>(1.81 ± 0.09) × 10^{-3}</td>
<td>3438</td>
<td>3.0 × 10^{-3}</td>
</tr>
<tr>
<td>$4_1$</td>
<td>5.30 ± 0.02</td>
<td>(1.99 ± 0.09) × 10^{-3}</td>
<td>2353</td>
<td>3.7 × 10^{-3}</td>
</tr>
</tbody>
</table>

"The data were obtained by simulating polymers in an unconfined MPC liquid."
In contrast, when HIs are included, as in our case via the MPC solvent, the friction is proportional to \( \zeta \approx \eta R_{H} \) with \( \eta \) being the viscosity of the solvent and \( R_{H} \) the hydrodynamic radius.\(^{17,39}\) As \( R_{H} \) varies with topology, diffusivities in bulk are distinct for \( 0, 3_{1} \) and \( 4_{1} \) knots, with the most complex (simplest) knot diffusing the fastest (slowest), as shown in the inset of Figure 3. Thus, in bulk and dilute solution, HIs are of utmost importance.

Next, we investigated the equilibrium properties in confinement. To evaluate the optimal constriction radius \( R_{\min} \), the diffusivities in longitudinal direction \( D_{L} \) were measured at fixed \( R_{\max} = 9a_{0} \) as a function of \( R_{\min} \) as shown in Figure 3. All modulated channels consisted of four chambers (compare Figure 1b). In doing so, we prevented spurious self-interactions of polymers when applying periodic boundary conditions in axial direction. To measure diffusivities, we followed closely the approach in ref 11 and determined \( D_{L} \) as a function of the narrowing radius \( R_{\min} \). In all setups, \( R_{\max} = 9a_{0} \). The inset shows the diffusion coefficient in bulk for all three topologies.

**Figure 3.** Diffusion coefficient in longitudinal direction \( D_{L} \) as a function of the narrowing radius \( R_{\min} \). In all setups, \( R_{\max} = 9a_{0} \). The inset shows the diffusion coefficient in bulk for all three topologies.

4. CONVECTIVE TRANSPORT IN CORRUGATED NANOCANNEALS

We characterize the resulting flow strength by the steady-state fluid flow velocity \( v_{F} \), which is directly proportional to the applied force \( f \), as shown in Figure 2. Figure 4a,b shows the transport velocity \( v_{P} \) of all polymer topologies as a function of the fluid flow velocity \( v_{F} \). At small fluid velocities, \( v_{P} \) is distinct for distinct topologies, whereas as soon as \( Pe > 1 \), these differences fade. The polymer velocity is increasing monotonically with \( v_{F} \) but not linearly; in contrast, \( v_{F} \) is a linear function of \( f \). Table 2 summarizes the applied body force \( f \), fluid velocity \( v_{F} \), polymer velocity \( v_{P} \) and Peclet numbers \( Pe \). Figure 4c,d shows the transport velocity of the \( 3_{1} \) and \( 4_{1} \) topologies with respect to the unknot as a function of fluid velocity \( v_{F} \). When the Peclet number of the \( 3_{1} \) or \( 4_{1} \) knots is smaller than unity, the unknot is transported faster by up to 1 order of magnitude compared to knotted structures, enabling a reliable separation of topologies for both constriction radii. Here, we take as a criterion for reliable filtering at least a twofold difference in \( v_{P} \).

**Figure 4.** Average transport velocities of knotted rings, \( v_{P} \), in units of \( a_{0} \), are shown in (a,b), average polymer velocity \( v_{P} \) as a fraction of the transport velocity of the unknot \( v_{U} \), in (c,d), and the ratio of transport velocity of the figure-of-eight knot to the trefoil knot \( v_{v_{F}/v_{4_{1}}} \), in (e,f), in all plots as a function of the average fluid velocity \( v_{F} \). (a,b,c,e) are the results for a constriction radius of \( R_{\min} = 4a_{0} \) and (b,d,f) \( R_{\min} = 5a_{0} \). Arrows show the polymer velocity at \( Pe = 1 \), \( v_{v_{F}/v_{4_{1}}} \), and dashed lines indicate the corresponding fluid velocity for every topology.
between knotted and unknotted states, a separation of distinct knotted topologies could be achieved at low flow strengths.

In contrast to other separation techniques, our proposed setup allows for a separation of dilute mixture of distinct ring polymer topologies without any pre- or posttreatment. The species, for instance, must be separated by mechano-chemical means in gel electrophoresis, which additionally is restricted to charged polymers of relatively short length. Furthermore, these channels offer the possibility of an easy upscaling by arranging several of them in an array.

For both radii, separation works most efficiently under the condition that Peclet numbers of all but one topology are smaller than unity. For higher Peclet numbers, polymers are prevented from exploring all degrees of freedom in radial direction. This effectively eliminates the free energy barrier across chambers, leading to a topology-independent transport.

Figure 5 qualitatively shows how flow erodes the free energy barrier and equalizes the CoM distribution. For every topology, the axial and radial CoM positions are shown against the sketched outline of the channel. For $Pe < 1$, all topologies show a strong preference to be located at the midpoints of the chambers, where $R(x) = R_{\text{max}}$. With increasing flow strength, this preference is diminished, and the CoM populates the position of the narrowing, indicating an enhanced mobility of every topology. Even though for $Pe > 1$ the CoM is more frequently located at the constrictions compared to smaller Peclet numbers, the 3t and 4t topologies are still likely to have their CoMs at the midpoints, explaining even at $Pe > 1$ a distinct transport velocity in Figure 4c.

Flow does not only influence the CoM position distribution but shows as well a strong influence on single molecule conformations. The shape of macromolecules, for example the span $S$ (see eq 5), reacts highly sensitively to Peclet numbers. Figure 6 shows the probability that the rings have a certain longitudinal span, $P(S)$, for polymers of different topologies for the constriction radius $R_{\text{min}} = 4a_0$. Lighter colors are used for increasing Peclet numbers.

Figure 5. Radial and longitudinal CoM positions sampled at time intervals $\Delta = 500t_0$ over a time span of duration $t = 2.28 \times 10^7t_0$. Shown data are for all topologies and flow strengths in a channel of $R_{\text{min}} = 4a_0$. Longitudinal periodic boundary conditions apply. Gray shaded regions correspond to $Pe \leq 1$. The upper row, $v_F = 0$, is for the equilibrium (passive transport) case. $v_F$ values are given in units of $10^{-3}a_0^{2}t_0^{-1}$.

Figure 6. Probability distributions of the longitudinal span, $P(S)$, for polymers of different topologies for the constriction radius $R_{\text{min}} = 4a_0$. Lighter colors are used for increasing Peclet numbers.

Table 2. Summary of the Average Fluid Velocity $v_F$ and Peclet Number $Pe$ of Distinct Topologies as a Function of Applied Body Force $f$ Used To Create the Flow

<table>
<thead>
<tr>
<th>$R = 4a_0$</th>
<th>$v_F$ [$10^3 a_0^{2}t_0^{-1}$]</th>
<th>$Pe = 10^{-3} a_0^{2}t_0^{-1}$</th>
<th>$R = 5a_0$</th>
<th>$v_F$ [$10^3 a_0^{2}t_0^{-1}$]</th>
<th>$Pe = 10^{-3} a_0^{2}t_0^{-1}$</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.02</td>
<td>0.187 $\pm$ 0.001</td>
<td>0.86 $\pm$ 0.04</td>
<td>0.02</td>
<td>0.154 $\pm$ 0.002</td>
<td>0.61 $\pm$ 0.04</td>
</tr>
<tr>
<td>0.04</td>
<td>0.303 $\pm$ 0.002</td>
<td>1.67 $\pm$ 0.21</td>
<td>0.04</td>
<td>0.203 $\pm$ 0.003</td>
<td>0.86 $\pm$ 0.04</td>
</tr>
<tr>
<td>0.06</td>
<td>0.661 $\pm$ 0.004</td>
<td>4.17 $\pm$ 2.22</td>
<td>0.06</td>
<td>0.55 $\pm$ 0.04</td>
<td>3.42 $\pm$ 2.02</td>
</tr>
<tr>
<td>0.10</td>
<td>1.02 $\pm$ 0.03</td>
<td>6.84 $\pm$ 4.50</td>
<td>0.10</td>
<td>1.18 $\pm$ 0.03</td>
<td>7.35 $\pm$ 5.54</td>
</tr>
<tr>
<td>0.20</td>
<td></td>
<td></td>
<td>0.20</td>
<td>1.76 $\pm$ 0.02</td>
<td>11.51 $\pm$ 8.47</td>
</tr>
</tbody>
</table>

*Gray shaded cells highlight Peclet numbers smaller than unity. Note that not all values of the body force $f$ were applied to every constriction radius.
c for $R_{\text{min}} = 4a_0$ and $\frac{1}{4}$ for $R_{\text{min}} = 5a_0$ as a function of the CoM position along the channel axis $x$, projected into a single chamber. For polymers in equilibrium and bulk, this parameter is unity; as soon as it starts stretching out longitudinally because of confinement or flow in axial ($x$) direction, it exceeds unity. A common feature in Figure 7a–f is that at $x = 0$ the polymer is the closest to being point-symmetrically distributed in space on average, whereas at the position of the constriction, the polymer is most elongated along the channel axis. Furthermore, increasingly strong flows result in a stronger shape deformation at $x = 0$, that is, $2G_{yy}/(G_{xx} + G_{yy}) > 1$, and less deformation at the narrowing $|x| = 9a_0$. Taking these two effects together, polymers show at high fluid flow velocities less changes in their shape across the chamber, compared to equilibrium. One can ascribe this to the lack of time to fully relax back to the equilibrium shape. Comparing distinct topologies, it is evident that the unknot can deform much more along a chamber, compared to knotted structures, which are hindered to do so by their essential crossings (see Figure 7).

While investigating the impact of the narrowing on the shape deformation, we must distinguish two cases; when the CoM is located at $x = 0$, the polymer is less deformed in the channel. For polymers in equilibrium and bulk, this parameter when located at $|x| = 9a_0$ (compare Figure 7a,b,c to d,e,f).

5. KNOT CONFORMATIONS AND MODES OF TRANSLOCATION

For both radii, we identified the Peclet number as the limiting factor for a successful topological separation. Interestingly, a constriction radius of $R_{\text{min}} = 5a_0$ is slightly larger than the bulk radius of gyration of the knotted portion of rings with 31 and 41 topology, whereas $R_{\text{min}} = 4a_0$ has approximately the same size as the aforementioned radius, when disregarding the repulsive wall potential. Figure 8 shows the knot gyration radius as a function of the CoM projected onto the longitudinal axis of a single chamber. The steric hindrance imposed by the $R_{\text{min}} = 4a_0$ for translocation can be deduced by the data shown in Figure 8a,b. Comparison of Figure 8a,b against c,d reveals that for $R_{\text{min}} = 5a_0$ the knot hardly changes size, whereas for the smaller narrowing, the knot has to shrink significantly to translocate; this shrinking represents an additional entropic barrier. Comparing the 41 knot to the 31 knot indicates that rings with the more complex knot topology are slightly larger and shrink less. As for the shape parameter, the average knot size becomes more uniform with increasing flow strength, accelerating translocation.

As the narrower constriction imposes a strong confinement and high hindrance to the part containing the essential crossings, its compression represents a non-negligible, additional entropic penalty. Taking into account the results of nanopores, which can block the translocation of the knotted portion when their radius, $R_{\text{min}}$ is comparable to the size of a monomer, it is surprising that different topologies can be
separated regardless of whether the ratio of knot size to constriction radius is smaller or larger than unity.

The severe restrictions imposed on the knots by $R_{\text{min}} = 4a_0$ manifest themselves in the probability distribution of knot length, $P(I_K)$, shown in Figure 9a,b. At high flow strengths, when the knot passes more frequently through the narrowings, cf. Figure 5, the $I_K$ distribution no longer increases but also shifts toward smaller values, a combined consequence of confinement and tightening due to shear.41 For the case $R_{\text{min}} = 5a_0$, depicted in Figure 9c,d, we likewise observe a reduction of the average knot length when $Pe > 1$; however, the wider constriction exerts less influence on knot size, whereas the effect due to shear is larger as polymers have higher Peclet numbers.

To investigate how the knotted region interacts with the constrictions, we examined the longitudinal positions of the CoM and the CoM at various translocation stages. When CoM and KCoM are in the same chamber, denoted as $n_C = n_K$, the CoM can translocate into the adjacent chamber, described as $\cap C$, and, occasionally, subsequently pulls the KCoM into this chamber to complete in this way the translocation, the pulling event denoted as $K \rightarrow C$. Being exclusively a two-step process, the probability of its occurrence is computed from the composition of the probabilities of the two elementary events, $P(\overline{K} \cap C \cap \overline{C} \cap n_C = n_K)$. The relative importance of this CoM-led translocation event compared to the knot leading the crossing motion is given by the ratio $\mu$

$$\mu = \frac{P(\overline{K} \cap C \cap \overline{C} \cap n_C = n_K)}{P(C \cap \overline{K} \cap n_C = n_K)}$$

(9)

Clearly, $\mu > 1$ indicates a translocation dominated initially by CoM pulling KCoM behind. Conversely, if $\mu < 1$, KCoM translocates first. Here, we defined the probability of an event as the fraction of such events of the whole trajectory. Note that the probability can depend on the time interval with which trajectories are sampled. For a robust calculation of the probability, we used a time interval of 0.1$t$, where $t$ is the longest relaxation time of each topology (see Table 1).

Figure 10 shows the ratio, $\mu$, as a function of flow strengths for the two constriction radii, revealing an opposite tendency only determined by $R_{\text{min}}$. For $R_{\text{min}} = 4a_0$ (solid lines), translocation is in the vast majority of cases led by CoM dragging KCoM behind at all flow strengths. For this constriction radius, the knot has to shrink to translocate and subsequently expands upon entering a new chamber, as shown in Figure 8a,b. The behavior associated with the rare scenario of the knot leading to translocation is consistent with the effects of a backflow created by the effectively denser knotted region and acting on the trailing unknotted portion. This backflow will in addition hinder a subsequent translocation of CoM,41,42 thus reinforcing the incidence of the CoM-led process.

Surprisingly, a modest enlargement of the constriction to $R_{\text{min}} = 5a_0$ completely changes the behavior of $\mu$ and hence the balance of the two translocation modes. Low flow strengths ($Pe \leq 1$) favor KCoM-led translocations, whereas for $Pe > 1$, there is no preference of KCoM- over CoM-led modes and $\mu \approx 1$. Here, the radius $R_{\text{min}}$ is slightly larger than the average knot gyration radius, thus the essential crossings impose only a minor additional hindrance. Hence, the average knot size is rather constant across a chamber (see Figure 8c,d), and transport can occur without requiring excessive shrinking and expansion of the knot. For $Pe \leq 1$, translocation is initiated by a subpart of the polymer diffusing into an adjacent chamber. Because the knot represents a significant fraction of the whole polymer, this explains the dominance of a knot-led process. This mechanism breaks down at high flow strengths, when motion is governed by convection, resulting in $\mu \approx 1$. The aforementioned backflow acts in the case of the larger constriction as well and explains the delay of knotted structures versus the unknot.

To investigate the translocation process in more detail, we examined the vector $w_{\text{KCoM} \rightarrow \text{CoM}}$ pointing from KCoM to CoM. We looked at the probability distribution $P(\phi)$ of the angle $\phi$ subtended between the flow direction and $w_{\text{KCoM} \rightarrow \text{CoM}}$. This distribution is averaged over all possible positions along

![Figure 9](image-url) Normalized probability distribution $P(I_K)$ of the knot length $I_K$ in a channel of narrowing $R = 4a_0$ in the case of a trefoil $3_1$ (a) and $4_1$ knot (b). The same quantity is depicted for a constriction radius $R_{\text{min}} = 5a_0$ for the $3_1$ (c) and $4_1$ (d) knots. With lightening of color, the average fluid flow velocity increases.

![Figure 10](image-url) Ratio $\mu$ of the probability that translocation is led by CoM over it being led by KCoM. Solid lines show results for $R_{\text{min}} = 4a_0$ and dashed–dotted lines for $R_{\text{min}} = 5a_0$. 

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the channel axis. Thus, at low flow strength, when the knot rarely translocates, it is dominated by configurations, when the polymer is close to the center of the chamber at \( R(x) = R_{\text{max}} \). In such a scenario, there is no preferred orientation. Thus, the distribution of \( \phi \) is rather uniform. At high flow strength, we see in Figure 11a,b for \( R = 4a_0 \) a strong preference for small angles, corresponding to a preferred orientation led by CoM, whereas in 11c,d, the distribution is bimodal with modes at \( \phi \approx 0 \) and \( \phi \approx 180^\circ \). Note that this distribution is based on all orientations of \( w_{\text{KCoM-CoM}} \) in the whole simulation and not only the ones during a translocation process, which explains why Figure 11c,d is not a symmetric bimodal distribution at high flow strengths.

6. CONCLUSIONS

We have examined the hydrodynamic transport of knotted ring polymers through nanochannels with a periodic hourglass topography. As a proof of concept, we have focused in this work on the three simplest knot types: the unknot, trefoil, and figure-of-eight knots. We established that the average transport velocities of different knot types can differ by up to an order of magnitude as long as flows with \( Pe < 1 \) are used. In this regime, transport can occur in two different modes, depending on whether the knotted or unknotted portion of the rings leads the motion through the constrictions. Remarkably, both modes allow for the efficient topological sorting of ring polymers. Increasing the flow velocity further, such that \( Pe > 1 \) for every topology, obliterates the topology-dependent component of the transport process, destroying any possibility of reliably separating a topological mixture. The loss of the topology-dependent response occurs when the convective flow is strong enough that polymers cannot relax and adjust to the local modulations of the channels. We hypothesize that differences in transport velocities will be observable for ring polymers with more complex topologies than considered here. As a part of future work, it will be particularly interesting to address systematically how these differences depend on the crossing number, a standard measure of complexity of knots, as well as their twist or torus character, which affects the translocation compliance through narrow pores and the mean displacement of the knot in elongational flow fields. The simplest way to address the latter point would be through a comparison of \( S_3 \) and \( S_5 \) knotted rings, which have the same nominal complexity but belong to the family of torus and twist knots, respectively. The results shed a new light on the out-of-equilibrium response of entangled polymers in spatial confinement, and we expect them to be useful to inform the design of new types of nanofluidic setups for the continuous topological sorting of polymers.

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Notes

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